

Příjemce:  
MV-GŘ HZS ČR -Technický ústav požární ochrany  
VŠCHT Praha, Fakulta chemicko-inženýrská  
ČVUT v Praze, Fakulta strojní

Poskytovatel: Česká republika - Ministerstvo vnitra

Projekt s názvem:

**Zvýšení bezpečnosti zásahových žebříků pro hasiče**  
s identifikačním kódem VI20162020021

Název předkládaného výsledku:

## **Structure and Mechanical Properties of Aluminium Alloy Sampled from a Firefighter Ladder**

Typ výsledku dle UV č. 837/2017	Evidenční číslo (příjemce)	Rok vzniku
<b>J<sub>sc</sub></b>	576/21	2017
ISBN-ISSN	Webový odkaz na výsledek	Kde a kdy publikováno
1213-2489	<a href="https://www.hzscr.cz/clanek/menu-vyzkum-a-vyvoj-vyzkumne-projekty.aspx">https://www.hzscr.cz/clanek/menu-vyzkum-a-vyvoj-vyzkumne-projekty.aspx</a>	Manufacturing Technology, 12/2017

### **Anotace výsledku:**

Žebříky pro hasiče jsou vyrobeny z hliníkové slitiny AA 6063. Tyto žebříky jsou široce používaným technickým nástrojem pro hašení požárů, pro zasahující hasiče a pro záchráněné osoby. Kvalita žebříků je kontrolována tzv. „Uživatelskou zkouškou“, což je nedestruktivní zkouška průhybem definovaná ČSN EN 1147. Bohužel tato zkouška není z hlediska bezpečnosti dostatečně přesvědčivá. Proto je projekt nazvaný „Zvýšení bezpečnosti zásahových žebříků pro hasiče“ (VI20162020021) zaměřen na komplexní posouzení stávajících hasičských žebříků a to prostřednictvím matematického modelování, materiálové analýzy a reálných zkoušek. V současné práci je představena struktura a mechanické vlastnosti vzorků (hliníková slitina AA 6063) odebraných z různých oblastí zásahových žebříků. Získaný výsledek potvrzuje vynikající mechanické vlastnosti vybraných vzorků, jako je mez kluzu v tahu a mez pevnosti v tahu, při laboratorní teplotě, ale obrovský pokles těchto vlastností po vystavení teplotám nad 200 °C i na krátkou dobu. To má za následek nutnost kontrolovat teploty v blízkosti žebříku, zejména v případě, že je žebřík umístěn v blízkosti plamene.

### **Řešitelský tým:**

**Ing. Jan Karl, Ing. Václav Vystrčil, Ing. Romana Friedrichová, Ph.D.,  
Ing. Ondřej Suchý, Ph.D., Lukáš Kotrc,  
prof. Dr. Ing. Dalibor Vojtěch, Ing. Jiří Kubásek, Ph.D.,  
Ing. Filip Průša, Ph.D., Ing. Klára Hosová,  
Doc. Ing. Miroslav Španiel, CSc., Ing. Karel Doubrava, Ph.D.**

- profiles. *Proceedings of the Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering Science* 228(12), pp. 2059-2067.
- [7] HOTAR, A., HOTAR, V. (2015). Fractal Geometry Used for Evaluation of Corrosion Resistance of Fe-14Al-6Cr Wt. % against Molten Glass. *Manufacturing Technology*, Vol. 15, No. 4, pp. 534-541.
- [8] Quantitative Fractography, *Fractography*. (1987), Vol. 12, ASM, s.356-398.
- [9] HRIVŇÁK, I. (1986). *Elektrónová mikroskopia ocelí*. Bratislava: Veda, 284 pages.
- [10] MÖSER, M. (1982). Elektronenmikroskopische Fraktographie, Elektronen-mikroskopie in der Festkörperphysik, Hrsg. H. Bethgeund J. Heydenreich, Berlin: VEB Deutscher Verlag der Wissenschaften, 1982, pp. 341-358.
- [11] MAHJANI, M. G., MOSHREFI, R., SHARIFI-VIAND, A., TAHERZAD, A., JAFARIAN, M., HASANLOU, F., HOSSEINI, M. (2016). Surface investigation by electrochemical methods and application of chaos theory and fractal geometry. *Chaos, Solitons and Fractals* 91, pp. 598-603.
- [12] NOVOTNÝ, J., HONZÍKOVÁ, J., PILOUS, V., STRÁNSKÝ, K. (2016). Verification for the causes of the degradation of welded joints in power plant. *Manufacturing Technology*, Vol. 16, No. 5, pp. 1106-1110.
- [13] LU, Ch. (2007) Some notes on the study of fractals in fracture, *Proceeding 5th Australian Congress on Applied Mechanics*, Brisbane, 2007, pp. 234-239.
- [14] KOBAYASHI, S., KOBAYASHI, R., WATANABE, T. (2016). Control of grain boundary connectivity based on fractal analysis for improvement of intergranular corrosion resistance in SUS316L austenitic stainless steel, *Acta Materialia* 102, pp. 397-405.
- [15] BROWN, C. A., HYDE, J. M., MONTGOMERY, J. (2014). Microscopy reveals effect of micro-electric discharge machining on stainless steel. *Laser Focus World* 50(7), pp. 49-52.
- [16] AHMADIAN, Z., DANAEI, I., GOLOZAR, M. A. (2014). Effect of surface treatment on corrosion resistance of 304 stainless steel implants in Tyrodesolution. *Archives of Metallurgy and Materials*, 59(1), pp. 25-30.
- [17] LIN, N., GUO, J., XIE, F., ZHANG, H., TANG, B. (2014). Comparison of surface fractal dimensions of chromizing coating and P110 steel for corrosion resistance estimation. *Applied Surface Science*, 311, pp. 330-338.

Paper number: M2017169

Copyright © 2017. Published by Manufacturing Technology. All rights reserved.

## Structure and Mechanical Properties of Aluminium Alloy Sampled from a Firefighter Ladder

Jiří Kubásek, Dalibor Vojtěch, Drahomír Dvorský

Department of Metals and Corrosion Engineering, University of Chemistry and Technology, Prague, Technická 5, 166 28 Prague 6, Czech Republic. E-mail: kubasekj@vscht.cz, vojtechd@vscht.cz

Firefighter ladders are manufactured of aluminium alloy AA 6063. These ladders are a widely used technical tool for firefighting, for intervening firefighters and for rescued persons. The quality of the ladders is checked by so-called "user test" which is a non-destructive deflection test defined by CSN EN 1147. Unfortunately, this test is not sufficiently conclusive in terms of safety. Therefore, the project called "Safety improvement of extension ladders for firefighters" (VI2016202021) is focused on the complex assessment of the existing firefighter ladders through mathematical modelling, material analysis and real testing. In the present work structure and mechanical properties of samples (aluminium alloy AA 6063) taken from different areas of a firefighter ladder are presented. The obtained result confirm excellent mechanical properties of selected samples, such as tensile yield strength and ultimate tensile strength, at laboratory temperature but a huge decrease in these properties after exposure to temperatures above 200 °C for even short times. This results in the necessity to control temperatures in the proximity of the ladder, especially in the case when the ladder is located near a flame.

**Keywords:** Aluminium alloy 6063, firefighter ladder, Electron microscopy, Mechanical characterization

### 1 Introduction

Aluminium alloys are widely used materials in automotive and aviation industry as well as for many specific applications which may require specific mechanical and

corrosion properties [1, 2, 3]. Aluminium alloy 6063 is one of the most widely used alloys for production of various components by extrusion [4]. The extrusion is commonly used to produce complex profiles. The main alloy-

ing elements of this alloy are magnesium and silicon giving it a medium strength. The alloy has a high corrosion resistance and is suitable for various surface treatments. The chemical composition of AA 6063 is given by ČSN EN 573-3 (Table 1). The values of selected mechanical properties in different states are then shown in Table 2.

Usually, the alloy is used in a thermally treated state. A T6 state is the most often one. This thermal treatment

consists of two steps. The first step is a solution thermal treatment designated as T4 that is performed in the range of 560 - 580 °C. In the T4 state the alloy exerts a good formability. Then, artificial aging and extrusion processes can be performed around 180 °C and 470 °C, respectively. AA 6063 is also suitable for welding and anodizing [5, 6, 7].

Tab. 1 Chemical composition (in wt.%) defined by ČSN EN 573-3.

Element	Mn	Fe	Mg	Si	Zn	Ti	Cr	Cu	others (each)	others (sum)	Al
[%]	max. 0.1	max. 0.35	0.45-0.9	0.20-0.6	max. 0.1	max. 0.1	max. 0.1	max. 0.1	max. 0.05	max. 0.15	Vol.

Tab. 2 Mechanical properties of AA 6063 alloy after different thermal treatments [5, 6, 7].

Thermal treatment	Wall thickness [mm]	TYS [MPa]	UTS [MPa]	Elongation A [%]	Elongation A <sub>50mm</sub> [%]	Brinell hardness
T4	≤ 25	65	130	14	12	45
T5	≤ 3	130	175	8	6	55
T6	3 - 25	110	160	7	5	50
	≤ 10	170	215	8	6	65
	10 - 25	160	195	8	6	60

The microstructure of the alloy may vary depending on the exact composition of the AA 6063 alloy which is often different depending on a particular material supplier. Microstructure of the as-cast ingots is characterized by cellular dendritic microstructure with large grain size. At grain boundaries segregation of secondary phases occurs. The precipitates at the grain boundaries are formed by intermetallic phases with Chinese font morphology ( $\alpha$ -Al-Fe-Si =  $Al_{13}Fe_3Si_{1-1.5}$ ) or needle-like morphology ( $\beta$ - $Al_3FeSi$ ). During thermal treatment, the original as-cast microstructure is removed. Microstructure of homogenized materials is generally composed of large grains and particles of secondary phases. During hot extrusion material is recrystallized. Microstructure of extruded products contains equiaxed grains as a consequence. In most cases, the precipitates present inside the grains correspond to the  $Mg_2Si$  phase and secondary phases distributed predominantly at the grain boundaries represent the intermetallic

phase (AlFeSi) [8, 9].

## 2 Materials and methods

### 2.1 Materials

Samples of aluminium alloy 6063 were taken from a new four-part firefighter ladder (Fig. 1) from different areas specified in Fig. 2. The ladder had been manufactured by extrusion of individual parts and subsequent composition and junction of these parts using TIG welding or riveting. Individual parts such as beams and rungs and also composed ladder were thermally treated at non-specified conditions which are manufacturer's internal secret. The proper chemical composition of AA 6063 alloy of which the studied ladder was prepared is shown in Table 3.

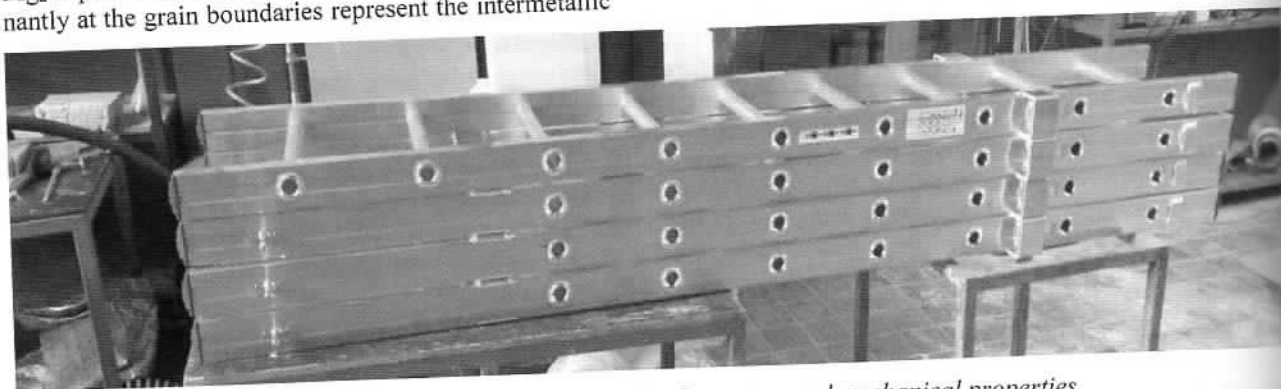


Fig. 1 Firefighter ladder used for study of structure and mechanical properties.

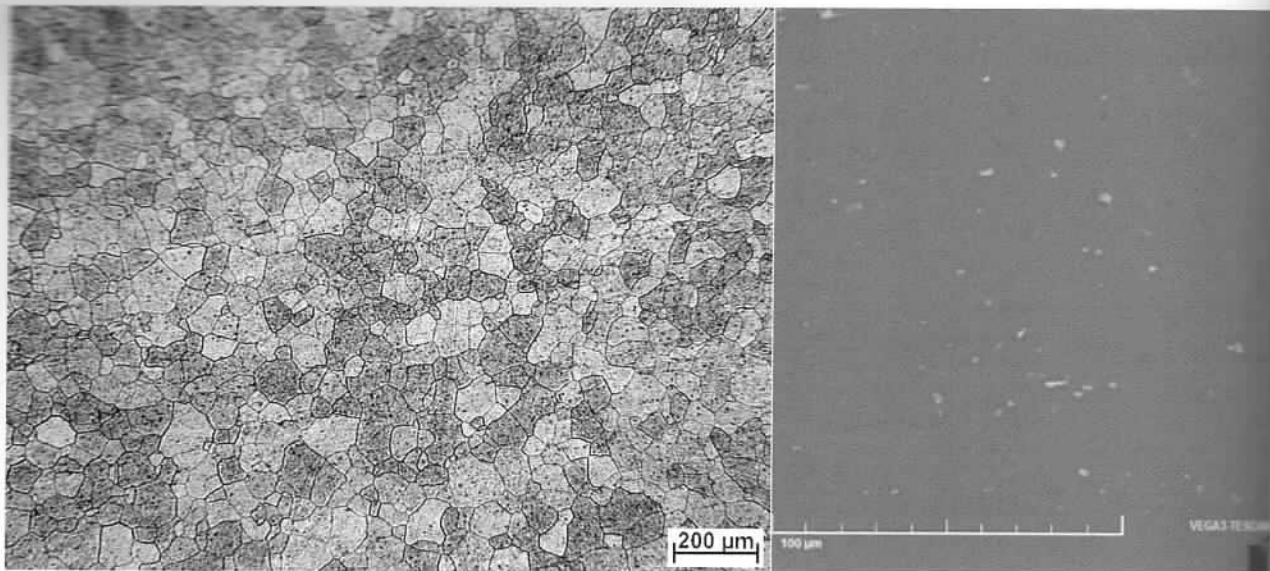


Fig. 3 Structure of a sample taken from the firefighter ladder: OM (left), SEM (right).

The Brinell hardness of the material was measured according to CSN EN ISO 6506-1 at all the sampling areas (Fig. 2) in both perpendicular and longitudinal direction. Obtained values were similar for all the measurements and correspond to  $80.0 \pm 1.1$  HBW62.5/2.5 in the perpendicular direction and  $77.8 \pm 2.4$  HBW62.5/2.5 in the longitudinal direction. Vickers hardness measurement according to the CSN EN ISO 6507-1 with a load of 1 kg (HV1) was performed along the whole cross section (Fig. 2) with no significant changes in the measured value. The average value and related standard deviation correspond to  $92.1 \pm 2.4$  HV1.

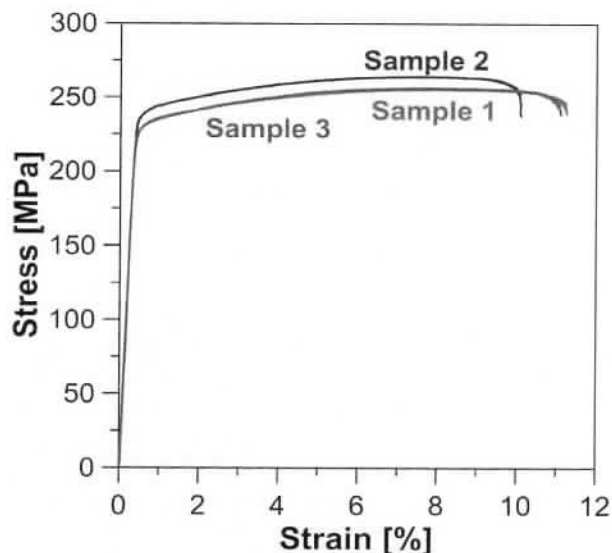


Fig. 4 Tensile stress-strain diagram reflecting similar mechanical properties of samples obtained from different areas of the ladder marked by numbers 1-3 (Fig. 2).

The samples for tensile tests were taken from the beams of the firefighter ladder according to the sampling in Fig. 2. Representative stress-strain curves of samples taken from different areas (1-3) are displayed in Fig. 4. The average values of tensile yield strength (TYS) and

ultimate tensile strength (UTS) supplemented by standard deviation are summarized in Table 4. It is evident that all the samples were characterized by comparable mechanical properties. The observed differences can be attributed to the condition of the samples surface, which has not been modified in any way and was therefore identical to the real surface of the firefighter ladder. Measured mechanical properties are also slightly higher compared to EN755-2 standard. It specifies that the material in T6 state (solution annealing + artificial aging) with a wall thickness of less than 10 mm has to reach TYS and UTS of 170 MPa and 215 MPa, respectively. In addition, elongation should correspond to at least 8% according to this standard. Thus, the studied material is characterized by enhanced mechanical properties compared to the standard. It can be attributed to the applied heat treatment processes which are unfortunately not published by the manufacturer.

The main strengthening mechanisms responsible for high values of mechanical properties of the presented aluminium alloy are strengthening by grain boundaries (Hall-Petch relation), strengthening by secondary phases and especially precipitation strengthening with a strong effect [4, 10].

According to the fracture morphology (Fig. 5), material is ruptured by intercrystalline plastic fracture. The plasticity of the fracture is evidenced by the presence of specific pits (holes) on the fracture surface. On the contrary, the fracture morphology does not contain facets which are the sign of a brittle fracture mode.

Tab. 4 Tensile mechanical properties (TYS = tensile yield strength corresponding to the 0.2 proof stress, UTS = ultimate tensile strength,  $A_{11.3}$  = elongation)

Sample designation*	TYS [MPa]	UTS [MPa]	$A_{11.3}$ [%]
1	$221 \pm 1$	$246 \pm 2$	$10.6 \pm 0.3$
2	$232 \pm 5$	$257 \pm 5$	$10.9 \pm 0.6$
3	$229 \pm 1$	$255 \pm 2$	$10.7 \pm 0.2$

\*reflects the sampling according to Fig. 2



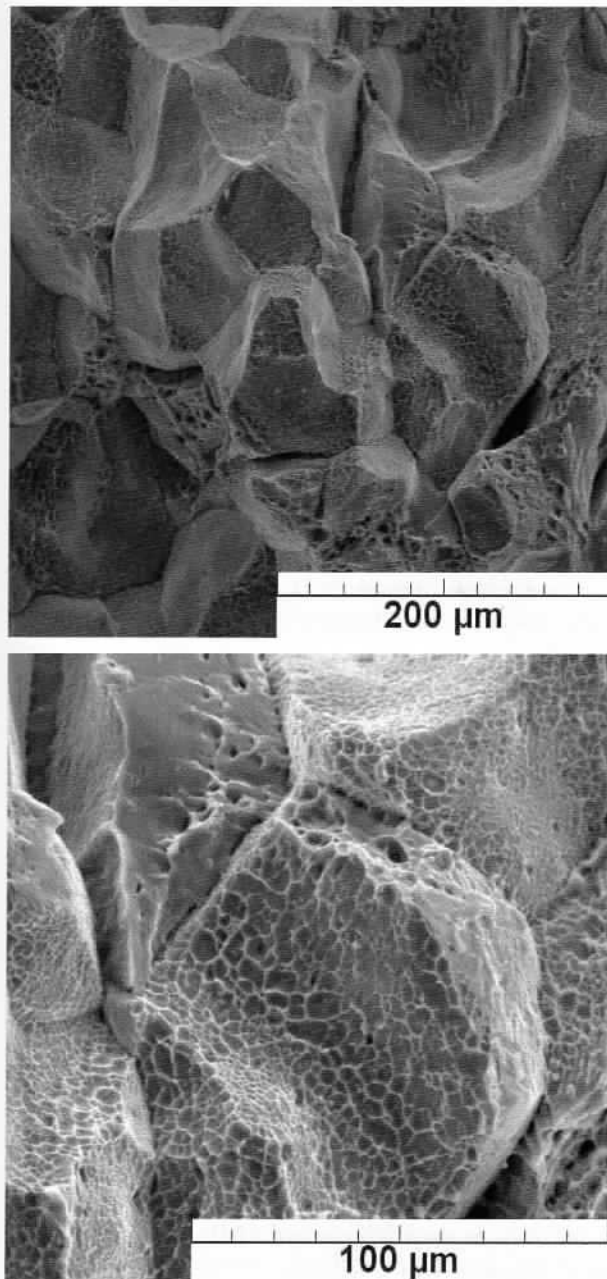


Fig. 5 Fracture area of sample 2 after tensile test (initial state).

Samples taken from area 2 (Fig. 2) were further thermally treated at different temperatures for 2 hours and subsequently stress-strain curves were measured at laboratory temperature. Representative curves are displayed in Fig. 6 and average values with standard deviation can be seen in Table 4. It is evident that short exposure of material to 200 °C has no effect on mechanical properties. However, increased temperatures cause strong decrease of both, TYS and UTS. Huge decrease is observed after exposure to 300 °C already. Elongation is improved at higher temperatures due to an increased plasticity of the material. Such behaviour can have catastrophic consequences if ladder is hit by heat near the flame, because firefighter ladders used in the Czech Republic have currently no temperature marks and the temperature close to the fire can easily exceed 300 °C.

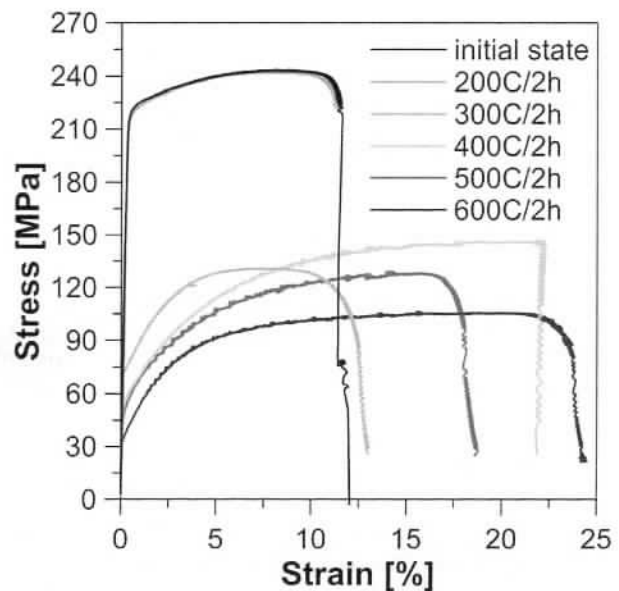


Fig. 6 Tensile stress-strain diagram reflecting mechanical properties of samples thermally treated at different temperatures for 2 hours.

Tab. 4 Tensile mechanical properties (TYS = tensile yield strength corresponding to the 0.2 proof stress, UTS = ultimate tensile strength,  $A_{11.3}$  = elongation) after the exposure to elevated temperatures.

Sample designation*	TYS [MPa]	UTS [MPa]	$A_{11.3}$ [%]
200°C/2h	219 ± 3	242 ± 4	10.4 ± 0.9
300°C/2h	75 ± 3	131 ± 2	12.3 ± 1.2
400°C/2h	59 ± 2	147 ± 3	21.7 ± 1.4
500°C/2h	38 ± 2	132 ± 2	17.7 ± 1.9
600°C/2h	43 ± 3	106 ± 4	22.2 ± 1.6

#### 4 Conclusion

Aluminium alloy 6063 is a well-known material with good mechanical properties, extrudability and corrosion resistance. Among other applications, it is also used for the manufacture of firefighter ladders which can be occasionally exposed to extreme conditions. In this study, specimens sampled from an exemplar ladder were characterized by quite high mechanical properties in tension (TYS ≈ 230 MPa, UTS ≈ 250 MPa,  $A_{11.3}$  ≈ 11 %). Such properties are assumed to be the result of thermal processing, especially artificial aging. Nevertheless, the study showed that the material is not stable at elevated temperatures. Even two hours of exposure at the temperature of 300 °C caused significant decrease of mechanical properties. That can represent a great risk, because in real application, the ladder can be exposed to such or even higher temperatures shortly but repeatedly, what can lead to the final failure. Therefore, temperature indicators are considered as a good improvement of the firefighter ladders.

## Acknowledgement

Authors wish to thank the Ministry of Interior (project: Safety improvement of extension ladders for firefighters - VI20162020021) and specific university research (MSMT No 20-SVV/2017) for the financial support of this research.

## References

- [1] LUŠTINEC, J., OČENÁŠEK, V., JELÍNEK, M. (2016). Structure of Al-Mg-Si cast and extruded rods for die forgings. In: *Manufacturing Technology*, Vol. 16, No. 5, pp. 1009-1013.
- [2] KOVALČÍK, T., STOULIL, J., SLÁMA, P., VOJTĚCH, D. (2015). The influence of heat treatment on mechanical and corrosion properties of wrought aluminium alloys 2024 and 6064. In: *Manufacturing Technology*, Vol. 15, No. 1, pp. 54-61.
- [3] LOU, S., WANG, Y., LU, S., SU, C. (2016). Extrusion process parameters optimization for the aluminum profile extrusion of an upper beam on the train based on response surface methodology. In: *Manufacturing Technology*, Vol. 16, No. 3, pp. 551-557.
- [4] SIDDIQUI, R. A., ABDULLAH, H. A., ALBELUSHI, K. R. (2000). Influence of aging parameters on the mechanical properties of 6063 aluminium alloy. In: *J Mater Process Tech*, Vol. 102, No. 1, pp. 234-240.
- [5] Aluminium Alloys - Aluminium 6063/6063A Properties, Fabrication and Applications. <http://www.azom.com/article.aspx?ArticleID=2812#2> (accessed 29.08.2017).
- [6] Understanding Extruded Aluminium Alloys. [https://web.archive.org/web/20031006212043/http://www.alcoa.com/adip/catalog/pdf/Extruded\\_Alloy\\_6063.pdf](https://web.archive.org/web/20031006212043/http://www.alcoa.com/adip/catalog/pdf/Extruded_Alloy_6063.pdf) (accessed 28.08.2017).
- [7] Alloy data sheet EN AW-6063 [AlMg0.7Si] <http://www.nedal.com/wp-content/uploads/2016/11/Nedal-alloy-Datasheet-EN-AW-6063.pdf>. (accessed 28.08.2017).
- [8] AYDI, L., KHLIF, M., BRADAI, C., SPIGARELLI, S., CABIBBO, M., MEHTEDI, M. E. (2015). Mechanical Properties and Microstructure of Primary and Secondary AA6063 Aluminum Alloy after Extrusion and T5 Heat Treatment. In: *Materials Today: Proceedings*, Vol. 2, No. 10, pp. 4890-4897.
- [9] ASENSIO-LOZANO, J., SUÁREZ-PEÑA, B., VANDER VOORT, G. (2014). Effect of Processing Steps on the Mechanical Properties and Surface Appearance of 6063 Aluminium Extruded Products. In: *Materials*, Vol. 7, No. 6, pp. 4224.
- [10] GAVGALI, M., TOTIK, Y., SADELER, R. (2003). The effects of artificial aging on wear properties of AA 6063 alloy. In: *Materials Letters*, Vol. 57, No. 24, pp. 3713-3721.

Paper number: M2017170

Copyright © 2017. Published by Manufacturing Technology. All rights reserved.

## The Effect of Annealing Temperature on Microstructure and Mechanical Properties of Lightweight Steel with Increased Aluminium Content

Ludmila Kučerová, Martin Bystrianský, Štěpán Jeníček  
Regional Technological Institute, University of West Bohemia in Pilsen, Univerzitní 8, 30614 Plzeň. Czech Republic. E-mail: skal@rti.zcu.cz, mbyst@rti.zcu.cz, jeniceks@rti.zcu.cz

A demand for enlightening of constructions in an automotive industry resulted in an intensive development of high strength steels and in attempts to decrease the weight of the steel by intensive alloying by lighter elements. The work used chemical concept of AHSS (advanced high strength steel) TRIP (transformation induced plasticity) steel with 0.2%C and micro-alloyed by 0.06%Nb and increased manganese content to 4% and aluminium to 6.5% to produce lightweight steel, which was cast and re-forged and subsequently annealed at various temperatures in the range of 300°C – 800°C. The resulting microstructures were analysed by light microscopy, laser scanning confocal microscopy, scanning electron microscopy and X-ray diffraction phase analysis and mechanical properties were measured by a tensile test. Tensile strengths in the region of 600 MPa – 757 MPa and total elongations around 20% were obtained for annealed samples.

**Keywords:** aluminium alloyed steel, light-weight steel, annealing, microstructure

Bibliografie článku:

**J<sub>sc</sub>**

KUBÁSEK J., VOJTĚCH D., DVORSKÝ D.: Structure and Mechanical Properties of Aluminium Alloy Sampled from a Firefighter Ladder. Manufacturing technology, December 2017, Vol. 17, No. 6, ISSN 1213-2489